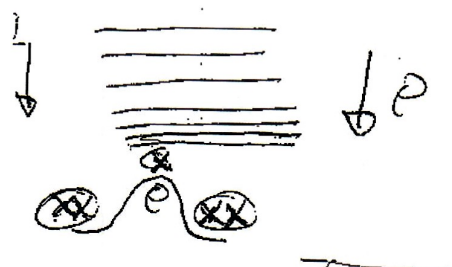


iii) Interchange Instability

(basic confinement consideration)

→ consider plasma confined by magnetic pressure gradient



$$\vec{\nabla} p = \vec{J} \times \vec{B} + \rho \vec{g}$$

$$\frac{dp}{dz} = -\nabla \left(\frac{B^2}{8\pi} \right) + \frac{\vec{B} \cdot \nabla B}{4\pi} + \rho g$$

$$\rho \ll 1$$

$$\boxed{-\nabla \left(\frac{B^2}{8\pi} \right) = \rho g}$$

$$\vec{g} = -g \hat{z}$$

$$\rho \rightarrow 0$$

equilibrium

$$\rightarrow \delta W = \int d^3x \left[\frac{Q^2}{8\pi} + (\vec{Q} \cdot \vec{E}) \delta \phi + \vec{j}_0 \cdot (\vec{E} \times \vec{g}) + (\vec{E} \cdot \nabla \rho) (\vec{Q} \cdot \vec{E}) - (\vec{E} \cdot \nabla \phi) \nabla \cdot (\rho \vec{E}) \right]$$

$$j_0 = 0$$

$$\rho_0 = 0$$

$$\delta W = \int d^3x \left[\frac{Q^2}{8\pi} + (\vec{E} \cdot \vec{g}) (\vec{E} \cdot \nabla \rho_0 + \rho_0 \nabla \cdot \vec{E}) \right]$$

Here, must address Q ,

$$\underline{Q} \equiv \underline{B}_0 \cdot \underline{\nabla} \underline{\Sigma} - \underline{\Sigma} \cdot \underline{\nabla} \underline{B} - \underline{B}_0 \underline{\nabla} \cdot \underline{\Sigma}$$

Now, can have $Q = 0$ if:

$$\rightarrow \underline{B}_0 \cdot \underline{\nabla} \underline{\Sigma} = 0 \quad \text{c.e.} \quad \underline{\Sigma} \text{ constant along } \underline{B}_0$$

and

$$\Rightarrow k_{||} = 0$$

$$\rightarrow \underline{\nabla} \cdot \underline{\Sigma} = - \frac{\underline{\Sigma} \cdot \underline{\nabla} \underline{B}_0}{B_0}$$

$\therefore$

$$\begin{aligned} dW &= \int d^3x \left[(\underline{\Sigma} \cdot \underline{g}) \rho_0 \left(\frac{\underline{\Sigma} \cdot \underline{\nabla} \rho_0}{\rho_0} - \frac{\underline{\Sigma} \cdot \underline{\nabla} B_0}{B_0} \right) \right. \\ &= \int d^3x \left[(\underline{\Sigma} \cdot \underline{g} B_0) \underline{\Sigma} \cdot \underline{\nabla} \ln(\rho/B) \right] \end{aligned}$$

$g < 0 \Rightarrow$ if $\nabla \ln(\rho/B) > 0$ anywhere

$\therefore$ instability there $\downarrow$

Now:

→ obvious parallel to Rayleigh-Taylor is

$$\nabla \rho > 0 \Leftrightarrow \boxed{\nabla \ln(\rho/B) > 0}$$

→ as $k_{||} = 0$, field lines not bent

so can think of instability motion as
interchange of flux tubes



Key question: Does interchange
lower/raise
potential energy?

interchange conserves magnetic flux

$$\Phi_2 = \int B_2 da = B_2 A_2$$

$$\Phi_1 = \int B_1 da = B_1 A_1$$

$$M_2 = \left(\frac{\rho}{B}\right)_2 \Phi_2$$

$$M_1 = \left(\frac{\rho}{B}\right)_1 \Phi_1$$

M m/length

but $\phi_1 = \phi_2 \Rightarrow$ Flux Frozen in!
(not equal $\rightarrow$ violation)

$$M_2 = (e/B)_2 \Phi$$

$$\text{so } \Delta M > 0 \Rightarrow \Delta (e/B) > 0$$

$\Rightarrow$ if e/B increases interchange will liberate gravitational potential energy, i.e.

instability, etc' $R-T_i$

$\Rightarrow$ Why care?

- (interchange) instability / severely degraded plasma confinement

- curing interchange stability is key element in device design $\rightarrow$ "minimum-B"

iv.) Interchange without Gravity — Expansion Free Energy

- in the context of magnetic confinement, "g" is a crutch, to represent

curved field lines

- r.e. 

$$a = \frac{v^2}{R_c} \rightarrow \underline{g}_{\text{eff}}$$

[centrifugal acceleration
on particle]

- Natural to investigate interchanges without
"g" $\Rightarrow$ pressure gradient drive
(expansion free energy)

- now

$$\delta W = \int d^3x \left[\frac{Q^2}{8\pi} + \gamma \rho (\nabla \cdot \underline{\epsilon})^2 + \underline{\epsilon} \cdot \nabla p (\nabla \cdot \underline{\epsilon}) + \underline{j} \cdot \underline{\epsilon} \times \underline{Q} \right]$$

[will pressure
gradient relax?]

Now, $\underline{Q} = 0 \Rightarrow$ avoid bending, etc.

$$\nabla \times (\underline{\epsilon} \times \underline{B}_0) = 0$$

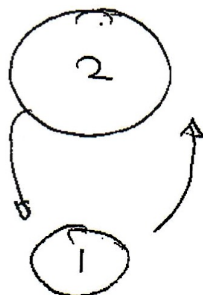
$$\Rightarrow \underline{\epsilon} \times \underline{B}_0 = \nabla \phi$$

$\hookrightarrow$ some scalar potential

and $\underline{B}_0 \cdot \nabla \phi = 0 \Rightarrow \phi$ constant along lines
of force ---

and can formulate dW in terms ϕ , or

$\Rightarrow$ consider interchange, with flux conservation



$$\Phi_1 = \Phi_2$$

Does interchange raise or lower energy?

$$\Delta E = [\text{final energy of } ①] - [\text{initial energy of } ①] \\ + [\text{final energy of } ②] - [\text{initial energy of } ②]$$

where interchange

- a) "puts" ① into ② slot
"puts" ② into ① slot

b) keeps $\underline{p p^{-\gamma} = p v^{\gamma} = \text{const.}}$

$V \equiv$ volume of flux tube

$$\Rightarrow \text{final energy of } ① \rightarrow (new P)_{\substack{\uparrow \\ \leftarrow P_1}} V_2 / (\gamma - 1) \\ \text{final energy of } ② \rightarrow (new P)_{\substack{\uparrow \\ \leftarrow P_2}} V_1 / (\gamma - 1)$$

so ...

$$\Delta E = \Delta W = \frac{1}{(\gamma-1)} \left[(p'_1 V_2 - p_1 V_1) + (p'_2 V_1 - p_2 V_2) \right]$$

$$\text{and } \left. \begin{aligned} p'_1 V_2 \delta &= p_1 V_1 \delta \\ p'_2 V_1 \delta &= p_2 V_2 \delta \end{aligned} \right\}$$

from eqn. state
 $p' \equiv$ pressures of
displaced
flux tubes
(argument akin to
Schwarzschild)

 $\Rightarrow$

$$(\gamma-1) \Delta W = \left\{ p_1 \left[\left(\frac{V_2}{V_1} \right)^\gamma V_2 - V_1 \right] + p_2 \left[\left(\frac{V_2}{V_1} \right)^\gamma V_1 - V_2 \right] \right\}$$

$$\begin{aligned} V_2 &= V_1 + \delta V \\ p_2 &= p_1 + \delta p \end{aligned}$$

$$\Delta W (\gamma-1) = \left\{ p_1 \left[\left(\frac{V_1}{V_1 + \delta V} \right)^\gamma (V_1 + \delta V) - V_1 \right] + (p_1 + \delta p) \left[\left(\frac{V_1 + \delta V}{V_1} \right)^\gamma V_1 - (V_1 + \delta V) \right] \right\}$$

$$\begin{aligned}
 (\gamma-1) \Delta W &= \left\{ P_1 V_1 \left[\left(1 + \frac{\delta V}{V}\right)^{-(\gamma-1)} - 1 \right] \right. \\
 &\quad \left. + P_1 V_1 \left(1 + \frac{\delta p}{p}\right) \left[\left(1 + \frac{\delta V}{V}\right)^\gamma - \left(1 + \frac{\delta V}{V}\right) \right] \right\} \\
 &= P_1 V_1 \left\{ \left[1 - (\gamma-1) \frac{\delta V}{V} + \frac{(\gamma-1)(\gamma)}{2} \left(\frac{\delta V}{V}\right)^2 - 1 \right] \right. \\
 &\quad \left. + \left(1 + \frac{\delta p}{p}\right) \left[1 + \gamma \frac{\delta V}{V} + \gamma \frac{(\gamma-1)}{2} \left(\frac{\delta V}{V}\right)^2 - 1 - \frac{\delta V}{V} \right] \right\} \\
 &= P_1 V_1 \left\{ -(\gamma-1) \frac{\delta V}{V} + \frac{(\gamma-1)(\gamma)}{2} \left(\frac{\delta V}{V}\right)^2 \right. \\
 &\quad \left. + \gamma \frac{\delta p}{p} - \frac{\delta V}{V} + \frac{\delta p}{p} (\gamma-1) \frac{\delta V}{V} + \gamma \frac{(\gamma-1)}{2} \left(\frac{\delta V}{V}\right)^2 \right\}
 \end{aligned}$$

$$\boxed{\Delta W = \gamma \left(\frac{\delta V}{V}\right)^2 + \frac{\delta p}{p} \frac{\delta V}{V}}$$

→ generic expression for
interchange dW

$$\gamma \frac{\delta V}{V} \left[\gamma \frac{\delta V}{V} + \frac{\delta p}{p} \right]$$

$$\frac{\delta p}{p} \text{ heat } \gamma \frac{\delta V}{V}$$

$$\delta W =$$

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clearly,

$$\frac{\delta V}{V} \sim (\nabla \cdot \underline{\underline{\epsilon}}) \quad , \quad \frac{\delta p}{p} \sim \underline{\underline{\epsilon}} : \nabla \underline{\underline{p}}$$

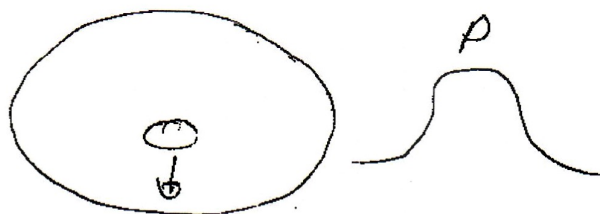
and

→ expansion free energy relaxation ⇒

$$\underline{\underline{\delta p < 0}}$$

→ i.e.

pressure
higher in
center so
collapse



$\delta p < 0 \Rightarrow$ relaxation

∴ key is sign

$$\frac{\delta V}{V}$$

$> 0 \rightarrow$ instability
(inflate)

$< 0 \rightarrow$ stability
(compress)

→ Now, for flute perturbation ($k_{||} = 0$)
Volume → B

$$V = \int S dl$$

$S \equiv$ cross-sectional
area of tube.



but $\Phi = B(l) S(l) = \text{const}$

$\Rightarrow$

$$\nabla = \Phi \int \frac{dl}{B} \quad \Rightarrow \quad \frac{\partial V}{\partial \nabla} < 0$$

$\Rightarrow$

$$\sigma \int \frac{dl}{B} < 0$$

$$\rightarrow \left[\begin{array}{l} \text{condition for interchange} \\ \text{stability} \quad (\sigma \uparrow \Leftrightarrow \text{displ.}) \\ \sigma \uparrow \quad \partial V > 0 \\ \quad \quad \quad \downarrow \quad \downarrow \\ \quad \quad \quad < 0 \quad < 0 \end{array} \right.$$

$\rightarrow$ content of criterion is that configuration should have a minimum in B in the core, to confine pressure

i.e.



then stable if

$$\sigma \int \frac{dl}{B} < 0$$

$\Rightarrow$ "minimum B " criterion for stability.

Min $B \rightarrow$ Max volume

→ if define $\psi \rightarrow$ label of surface enclosing const flux Φ



$\therefore V(\psi) \equiv$ volume enclosed by flux surface

$P(\psi) \equiv$ pressure enclosed

$dP/d\psi < 0 \Rightarrow$ need $\frac{dV}{d\psi} > 0$ expand
 $\nabla p \ll 0$
 $\uparrow$
 exp free energy
 $\leftrightarrow$ minimum-B Δ minimum

→ Can re-write instability criterion:

$$\begin{aligned} \delta W &= p_i \delta V \left(\gamma \frac{\delta V}{V_i} + \frac{\delta p}{p_i} \right) \\ &= p_i \delta V \left[\delta \ln(p V^\gamma) \right] \end{aligned}$$

so $\boxed{\delta(p V^\gamma) < 0} \rightarrow$ inst. (akin Schwarzschild)

Also, if tube $\odot$ has flux ψ , then

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$$v = u \psi$$

$\Rightarrow$

$$\frac{\delta w}{\psi} = \rho \delta u \frac{\delta(\rho u^{\delta})}{\rho u^{\delta}} < 0$$

$$\begin{aligned} \delta w &= \rho \delta v [\delta(\ln(\rho v^{\delta}))] \\ &= \rho \psi \delta u [\delta(\ln(\rho u^{\delta}))] \end{aligned}$$



→ What does it Mean?

$$V \underset{\substack{\uparrow \\ \text{volume}}}{=} \int dl A = \oint \frac{dl}{B}$$

now $\nabla p \rightarrow$ "expansion free energy"

$$\delta V > 0 \Rightarrow \delta \int \frac{dl}{B} > 0 \rightarrow \text{fluid element expands}$$

$\Rightarrow$ tends reduce W_p

$$\delta V < 0 \Rightarrow \delta \int \frac{dl}{B} < 0 \rightarrow \text{fluid element compresses}$$

$\Rightarrow$ tends increase W_p

$$\delta V > 0 \rightarrow \text{'maximum } B \text{'}$$

$$\delta V < 0 \rightarrow \text{'minimum } B \text{'}$$

Can then define:

$$E_p \equiv -p U, \quad U \equiv - \oint \frac{dl}{B}$$

$\oint$
potential
energy of tube

(i.e. for sign convention)

$\therefore$ can aque tube tends to move in direction of lower U .

$\rightarrow$ equilibrium for $p = p(U)$

then, not surprisingly, can develop parallel between convection and interchange

i.e.

Convection	Interchange
gravitational potential energy	$E_p \rightarrow$ expansion energy
blob	flux tube.
displace blob	displace tube
$\rho' < \rho_{\text{ambient}}$ $\rightarrow$ buoyant rise	$\frac{dV}{V} > 0$ $\rightarrow$ expansion continues ($\frac{d\rho}{d\eta} < 0$) (squeeze out)
adiabatic profile $\frac{d\rho}{\rho} = \gamma \frac{d\rho}{\rho}$	<u>adiabatic displacement</u> $-\gamma \rho \frac{\delta \eta}{\eta} = \frac{\delta \rho}{\rho} \delta \eta$
Schwarzschild Criterion $\frac{d\rho}{\rho} < \gamma \frac{d\rho}{\rho}$ for instability	Interchange Criterion $\frac{d\rho}{\rho} \delta \eta < -\gamma \rho \frac{\delta \eta}{\eta}$ $\Rightarrow \left \frac{d\rho}{d\eta} \right > \frac{-\gamma \rho}{\eta}$ ρ sufficiently steep $\rightarrow$ overcome comp.

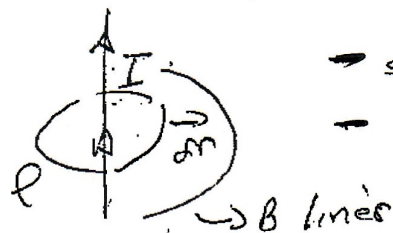
∴ for instability: $\left| \frac{dp}{du} \right| > \frac{\gamma p}{u}$
 $\downarrow$
 charge from relaxation $\rightarrow$ adiabatic pressure change

for stability, need:

$$\left| \frac{dp}{du} \right| < \frac{\gamma p}{|u|}$$

→ Consider some configurations (magnetic)

a) single wire



- stability to displacement dr
 - dp/p limit $\int$

now $\oint \frac{dl}{B}$

$$dl = 2\pi r$$

$$B = 2I/r$$

$$dl/B \sim \frac{\pi r^2}{I} \left[\begin{array}{l} \rightarrow \text{"wire is not"} \\ \text{"minimum } -B" \\ \text{ie. actually maximum} \\ \rightarrow \text{will have a } \underline{\underline{\text{opert.}}} \end{array} \right]$$

for νp limit: $\frac{dp}{d\psi} < \frac{\gamma p}{|U|}$

$$U \equiv -\int \frac{dp}{\rho} \sim -r^2$$

$$\frac{dp}{d\psi} = \frac{dp}{dr} \frac{dr}{d\psi}$$

U scalar $\Rightarrow$
 $\mathbf{I}$ cancels

$$= \left| \frac{dp}{dr} \right| \left(\frac{1}{2r} \right)$$

$$\Rightarrow \left| \frac{1}{\rho} \frac{dp}{dr} \right| < \gamma \frac{(2r)}{r^2}$$

$$\therefore \left| \frac{1}{\rho} \frac{dp}{dr} \right| < \frac{2\gamma}{r}$$

$$\Rightarrow \boxed{\left| \frac{d \ln p}{d \ln r} \right| < 2\gamma}$$

$\rightarrow$ imposes limit on pressure gradient for
 interchange stability. $\Rightarrow$ " β limits"

b.) can approach point dipole similarly $\rightarrow$ i.e. earth.
 i.e. $B \sim 1/r^3$
 $\Rightarrow U \sim r^4$
 $dh \sim r$

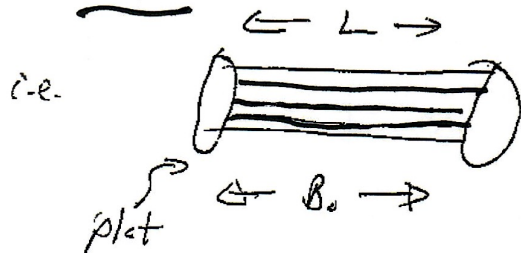
similar reasoning $\Rightarrow -\frac{d \ln p}{d \ln r} < 4\gamma$

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→ Line Tying and Conducting End Plates

→ Till now, have ignored boundary

→ consider plasma between two conducting end plates



$$\underline{E}_t = 0 \text{ on plate}$$

$$\Rightarrow \sum \left| \right|_{\text{plate}} = 0$$

$$\underline{E} + \underline{v} \times \underline{B} = 0$$

$$\underline{v}_t \approx \frac{c \underline{E}_t \times \underline{B}_0}{B_0^2}$$

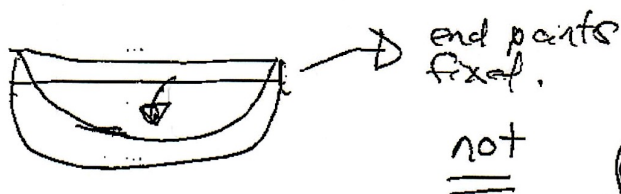
lines are "feed" ↓

c.e. displacement has form :

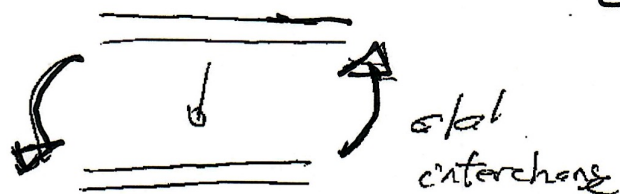
$$\underline{E}_t = 0, \underline{v}_t = 0$$

$$\partial_t \underline{E} = 0$$

$$\sum \left| \right|_{\mu} = 0$$



not



⇒ field lines bent ↓

now, $\underline{v}_0 \neq 0 \Rightarrow$

$$dW = \int d^3x \left[\frac{Q^2}{8\pi} + \gamma \rho (\nabla \cdot \underline{\underline{\epsilon}})^2 + (\underline{\underline{\epsilon}} \cdot \nabla \rho_0) (\nabla \cdot \underline{\underline{\epsilon}}) \right]$$

$$\underline{Q} = \nabla \times \underline{\underline{\epsilon}} \times \underline{B_0}$$

$$= \underline{B_0} \cdot \nabla \underline{\underline{\epsilon}} - \underline{\underline{\epsilon}} \cdot \nabla \underline{B_0} - \underline{B_0} \cdot \nabla \underline{\underline{\epsilon}}$$

$$\nabla \cdot \underline{\underline{\epsilon}} \neq 0$$

new stabilizing effect

$$dW = \int d^3x \left[\frac{(\underline{B_0} \cdot \nabla \underline{\underline{\epsilon}} - \underline{\underline{\epsilon}} \cdot \nabla \underline{B_0})^2}{8\pi} + \gamma \rho (\nabla \cdot \underline{\underline{\epsilon}})^2 + (\underline{\underline{\epsilon}} \cdot \nabla \rho_0) \nabla \cdot \underline{\underline{\epsilon}} \right]$$

i.e. can't take $\underline{B_0} \cdot \nabla \underline{\underline{\epsilon}} = 0$ any more!

so $Q \sim B_0 \frac{\partial \epsilon_r}{\partial z}$
new

i.e. can make $(\nabla \cdot \underline{\underline{\epsilon}}) B_0$
smaller ... $\frac{\partial \epsilon_r}{\partial z} \approx 0$

$$dW \sim V \left[\frac{B_0^2}{8\pi} \left(\frac{\partial \epsilon_r}{\partial z} \right)^2 + \underbrace{\gamma \rho \left(\frac{\partial u}{u} \right)^2 + \rho \frac{\partial u}{u}}_{\text{old}} \right]$$

i.e. schematic ...

$$\frac{\partial \epsilon_r}{\partial z} \sim \frac{\epsilon_r}{L}$$

$$\frac{\partial u}{u} = \frac{\partial u}{u} \epsilon_r$$

$$\rho = \rho \epsilon_r$$

→ heuristic:

$$\delta W \sim V \left\{ \left(\frac{\beta_0^2}{8\pi L^2} + \gamma \rho \left(\frac{\nabla \psi}{L} \right)^2 + \nabla \rho \frac{\nabla \psi}{L} \right) \epsilon^2 \right\}$$

∴ $\delta W < 0 \rightarrow$ instability $\Rightarrow$

instability if $-\frac{\nabla \rho \nabla \psi}{L} < \gamma \rho \left(\frac{\nabla \psi}{L} \right)^2 + \frac{\beta_0^2}{8\pi L^2}$

$\Rightarrow$ line tying raises
critical pressure gradient

δ
additional
stabilizing
effect

$\Rightarrow$ clearly stabilizing $\Rightarrow$ β limit!

Physics $\rightarrow$ fixing end points forces
bending of field lines

$\rightarrow$ loss : interchange structure

$\rightarrow$ energy expended coupling to
pulling magnetic field lines.

